

EXPERIMENTAL AND NUMERICAL INVESTIGATION OF V-SHAPED EPOXY ADHESIVE JOINTS

Mohd Afendi^{1,*}, Nur Athirah¹, M.S. Abdul Majid¹, R. Daud¹ and Tokuo Teramoto²

¹School of Mechatronic Engineering, Universiti Malaysia Perlis, 02600, Arau, Perlis
Phone : +604-9885162 ; Fax :+604-9885167

*Email: afendirojan@unimap.edu.my

²Graduate School of Systems and Information Engineering,
University of Tsukuba, 305-0821, Tsukuba, Japan

ABSTRACT

This paper deals with the stress and failure characteristics of V-shaped epoxy adhesive joints. The effect of scarf angles upon failure morphology was investigated by tensile tests and monitoring using high speed cameras. V-shaped specimens were fabricated with three bond thicknesses, t (i.e. 0.2mm, 0.6mm, and 1.0mm) and various scarf angles (i.e. $\theta = 30^\circ, 45^\circ, 60^\circ, 75^\circ, \text{ and } 90^\circ$). From failure surface observation, failure morphology can be divided into five types, consisting of interface failure and/or cohesive failure. Shear stress plays a major role in failure morphology where higher shear stress favors interface failure in the specimens tested. A simple failure criterion is also proposed based on the results obtained. It is found that the proposed criterion can approximately predict the failure stress of V-shaped epoxy adhesive joint specimens. For stress analysis, V-shaped epoxy adhesive joints having bond thicknesses $t = 1.0\text{mm}$, and with various scarf angles (i.e. $\theta = 30^\circ, 45^\circ, 60^\circ, 75^\circ, \text{ and } 90^\circ$), were modelled. Stress singularity observed in simulation plays a major role in failure morphology where higher singularity favors cohesive failure in the specimens tested in experiment.

Keywords: V-shaped; adhesive joint; bond thickness; scarf angle; failure criterion; finite element.

INTRODUCTION

Adhesive bonding is an important technique that has been used since ancient times. It is now being used widely in construction and industrial structures, etc (Bachtiar, Sapuan, & Hamdan, 2010; Ravi Sankar, Srikant, Vamsi Krishna, Bhujanga Rao, & Bangaru Babu, 2013). The exploitation of composite materials and adhesives has greatly increased because they offer lighter, more compact and higher performance structures. Adhesive bonding has various benefits: it covers a wide range of joins, and has the ability to join very thin sheet and small parts. With the application of adhesive bonding, the improvement of products and production processes also becomes possible (Jeffrey, Tarlochan, & Rahman, 2011; Salleh, Yusop, & Rosdi, 2013). However, adhesive bonding also has disadvantages, such as limited heat resistance and impossibility of non-destructive testing. Adhesive bonding is definitely an important parameter in structural design. It also has a significant impact on the reliability of a structure. It is therefore crucial to understand the influence of adhesives upon strength properties of bonded structures.

In previous studies, fracture testing of adhesive joints has been conducted using a room temperature curing two-part epoxy adhesive resin, which is widely used in general. Tensile tests were conducted by varying the thickness of adhesive layer and scarf angle, where a significant effect on fracture stress and the morphology of adhesive joint was revealed (Afendi & Teramoto, 2009, 2010; Afendi, Teramoto, & Bakri, 2011; Afendi, Teramoto, & Matsuda, 2011). In addition, experimental and numerical evaluation of scarf adhesive joints subjected to static loading has been discussed (He, Sawa, Iwamoto, & Hirayama, 2010). Nevertheless, less attention has been paid to investigating the strength of double scarf (also referred as V-shaped) adhesive joints, which thus motivates this study. In this study, tensile test specimens of V-shaped adhesive joints were manufactured using stainless steel as adherents. In comparison to scarf joints, V-shaped adhesive joints have relatively less eccentricity of effect. Tensile testing was carried out to investigate the effect of scarf angle and bond thickness upon strength properties, to examine the relationship between strength and fracture morphology, and to establish the fracture criterion involved. Meanwhile, stress analysis was conducted using finite element software to examine the relationship between stress distribution within adhesive layers and failure morphology.

EXPERIMENTAL PROCEDURES

In this study, a two-part room temperature curing epoxy adhesive resin (Hi-Super 30, produced by Cemedine, Co., Japan) was used. A V-shaped adhesive joint specimen was made of stainless steel (i.e. SUS304). Figure 1 shows the dimensions of the specimen. The mechanical properties of the materials are given in Table 1. The bonding surface was polished with sandpaper, so that the surface roughness was uniform for each specimen. The bond thickness, t was adjusted using a special jig ($t = 0.2\text{mm}$, 0.6mm , and 1.0mm). Various scarf angles, and θ were also considered (i.e. $\theta = 30^\circ$, 45° , 60° , 75° , and 90°). All specimens were cured at room temperature for more than 24 hours. After the specimens were totally cured, excessive adhesive was removed using a portable grinder and a sharp knife. The actual bond thickness, t was then measured with a digital microscope. The tensile test of the V-shaped specimen was conducted at room temperature using a universal testing machine (INSTRON) with $0.5\text{mm}/\text{min}$ crosshead speed, and 10kN maximum load. A summary of the experimental conditions is given in Table 2. Load and displacement were measured up to the failure point. Tensile tests were carried out at least eight times for each condition. In addition, some experiments on specimens with pre-mounted strain gauge were performed. During the experiments, failure paths were observed using a high speed camera. After the testing, failure surfaces was observed using a digital microscope and their failure morphology and pattern were recorded.

NUMERICAL ANALYSIS

Stress distribution in adhesive layers and bonding interfaces was analyzed using finite element analysis (FEA) ANSYS software. By taking advantage of symmetrical features on the y-axis, a half FEA model was considered, as shown in Figure 2. Adhesive bond thickness, t was 1.0mm . A two-dimensional FEA model had a width of 20mm and height of 160mm . Various scarf angles were also modelled. In all simulations, a tensile stress of 1MPa was applied in the y-direction on all nodal points at both ends of adherents. As for the prescribed boundary conditions, all nodal points at x-direction

were constrained. Stress values along bonding interfaces (i.e. ξ_1 and ξ_3) and at the center of the adhesive layer, ξ_2 were recorded, S and L were distance and interface length, respectively. A summary of the simulation conditions is given in Table 3.

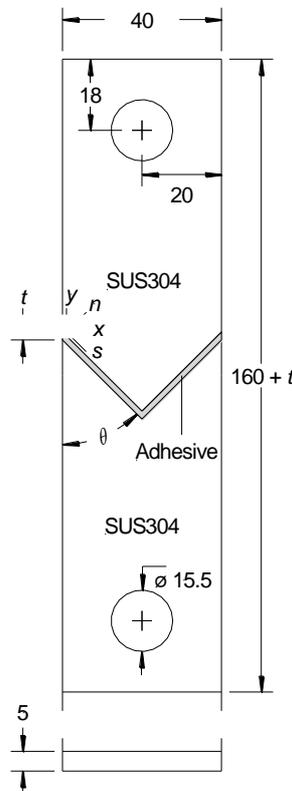


Figure 1. Geometry of V-shaped epoxy adhesive joint specimen.

Table 1. Mechanical properties of materials.

Material	E (Eitssayeam, Intatha, Rujijanagul, Pengpat, & Tunkasiri, 2006)	σ_y (MPa)	ν
Epoxy adhesive	3.4	34.76 (1.67)	0.39
SUS304*	197	307.8 (6.02)	0.3

* data taken from manufacturer's catalogue; () denotes the value of standard deviation.

Table 2. Experimental condition.

Parameter	Value
Adhesive angle, θ (degree)	90, 75, 60, 45, 30
Bond thickness, t (mm)	1.0, 0.6, 0.2
Number of specimen, n	8
Experimental temperature	Room temperature
Crosshead speed (mm/min)	0.5
Maximum load (kN)	10

have greater strength than those with interface failure. In this experiment, with regard to normal stress, when scarf angle was closer to 90° the interface failure as well as strength were increased. Since this experiment also showed a similar trend, it can be concluded that good results were obtained.

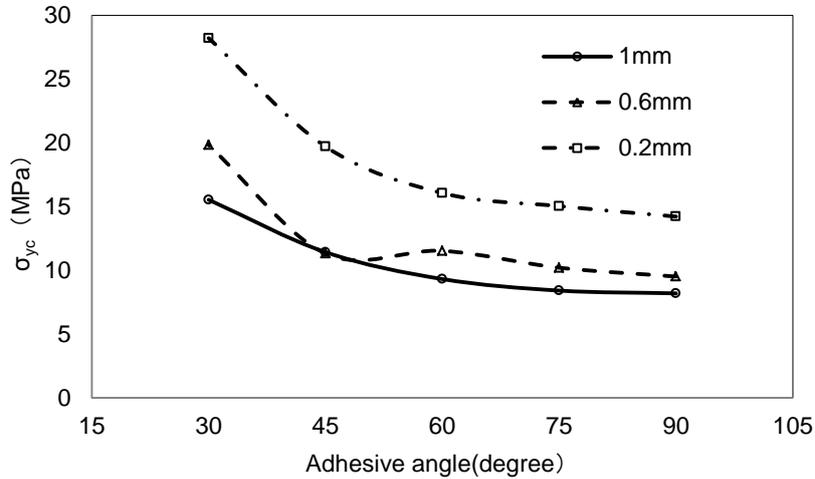


Figure 3. Nominal stress against scarf angle.

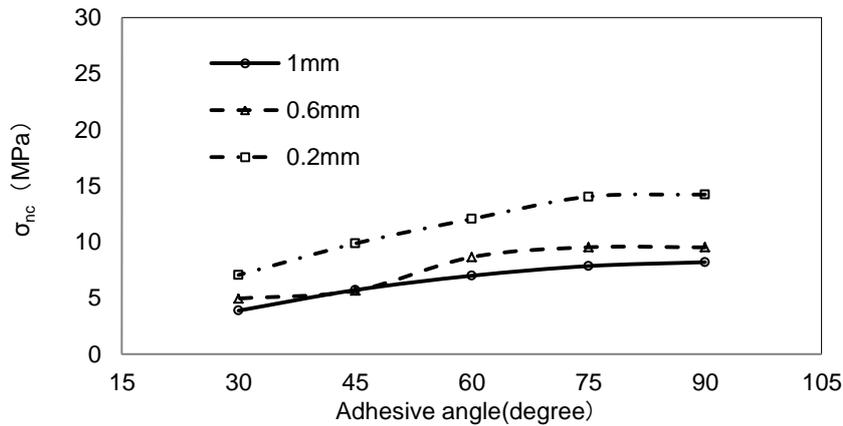


Figure 4. Normal stress against scarf angle.

Figure 5 shows the shear stress in the adhesive joint with regard to variation of scarf angle. It is also confirmed that the smaller the thickness of the adhesive layer, the higher the strength. In addition, in each bond thickness, the shear stress is increased if the scarf angle becomes more acute. When the scarf angle is more acute, the shear stress will increase and interface failure is likely to occur. Therefore, shear stress is thought to be a dominant factor in interfacial failure.

Failure criterion was then estimated from the experimental results. First, stress normal to the direction of the adhesive layer of the specimen at failure, and shear stress at failure are defined as σ_{nc} and τ_{snc} , respectively. Therefore,

$$\sigma_{nc} = \sigma_{yc} \sin \theta, \tau_{snc} = \sigma_{yc} \sin \theta \cos \theta \tag{1}$$

are defined. Thus, from the relation between σ_{nc} and τ_{snc} ,

$$\sigma_{nc}^2 + \tau_{snc}^2 = const \quad (2)$$

can be derived. Here, the shape of the specimen in the following relationship is considered

$$\sigma_y' L = \sigma_y W \quad (3)$$

where, σ_y' is the y-direction stress along the adhesive layer, σ_y is the nominal stress, L is the length of the adhesive layer, and W represents the width of the model. From Eqs. (2) and (3), the following relationship is then derived.

$$\sigma_{yc}' = \sigma_y \frac{W}{L} = \sigma_y \sin \theta = const \quad (4)$$

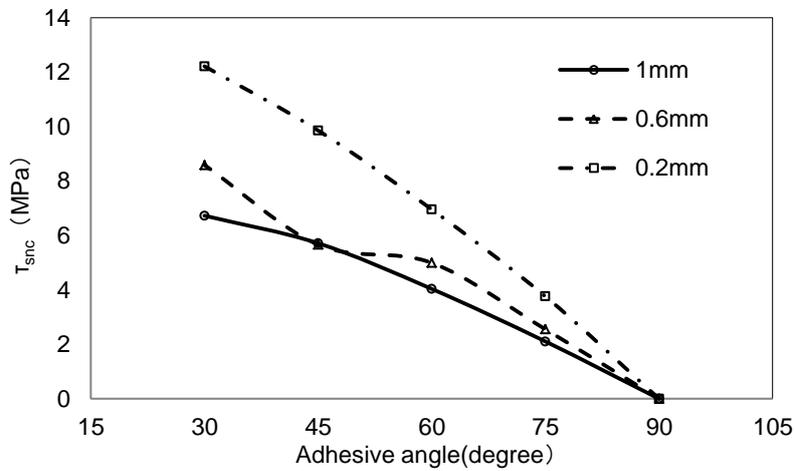


Figure 5. Shear stress against scarf angle.

Figure 6 shows the relationship between σ_{yc}' and t obtained in this study. From this result, it was observed that failure stress in the y-direction along the adhesive layer, σ_{yc}' is exponentially proportional to the bond thickness, t which can be expressed as follows

$$\sigma_{yc}' = mt^n \quad (5)$$

Here, m and n are constants which can be determined experimentally. The failure criterion expression of this experiment through power regression of line in Figure 6,

$$\sigma_{yc}' = 8.05t^{-0.35} \quad (6)$$

is now derived. From this form of failure criterion expression, for the particular material and shape geometry used in this investigation, it is considered that the failure can be roughly predicted. This can be seen in Figure 7 where the experimental data is in good agreement with the respective prediction lines. Thus, it can be concluded that for V-shaped adhesive joints, a simple failure criterion as in Eq. (6) is obtained.

Representatives of failure type and morphology observed from the specimen tests are given in Table 5. Basically, failure of specimens can be divided into five patterns: 100% interface failure, interface failure transition, cohesive-interface transition, rough cohesive failure and 100% cohesive failure. Interface failure is likely to occur in joint specimens with smaller scarf angles while cohesive failure is in higher scarf angles. This can be related to the contribution of shear stress within the joint specimen. The higher the shear stress component, the greater the possibility for interface failure to occur. Table 6 shows the representative failure surface for each scarf angle. It can be seen here that for 30° and 45°, interface or interface transition failures are dominant. However, for 60°, 75° and 90°, cohesive-interface transition and rough/pure cohesive failures are mostly observed. It is noteworthy that failure morphology also changes with bond thickness. For thin bond thickness, $t = 0.2\text{mm}$, a higher percentage of cohesive failure has been observed. This can be attributed to the increment of shear stress component in a thin adhesive layer.

Table 4. Value of σ_{yc} for strength prediction.

Scarf angle (degree)	Bond thickness, t (mm)		
	1.0	0.6	0.2
90°	8.1977	9.5170	14.2235
75°	8.1278	9.8613	14.5245
60°	8.0701	9.9871	13.9092
45°	8.0799	8.0063	13.9389
30°	7.7677	9.9158	14.1065
Average	8.0486	9.8203	14.1405

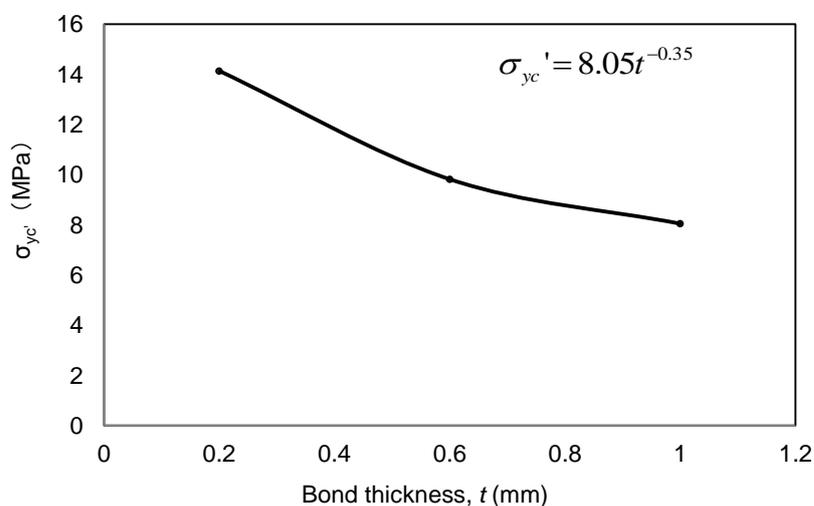


Figure 6. Failure stress-bond thickness prediction diagram.

From Figure 8, it can be seen that if scarf angle becomes slanted, bonding interface stress will be reduced. Moreover, stress singularity can be seen in models with 90° and 75° scarf angles. Stress singularity at bonding interfaces should therefore be considered. It has been reported that 90°, 75° and 30° joints will produce stress singularity, but for 45° and 60° joints, this singularity is significantly decreased. Theoretically, singularity in a 45° joint is relatively small. Due to this, a crack has great likelihood of originating either at tip B or edge C. Eventually, both cracks have great

potential to originate either at tip B or edge C. Eventually, both cracks will possibly intersect in the middle of the adhesive layer as can be seen in Figure 9 (a) which results in an interface transition type of failure. This can be appreciated by considering stress distribution in the specimen shown in Figure 9 (b). It is obvious that stress is high at tip B and edge C. Figure 10 shows applied load against strain for a 45° joint having three strain gages mounted. It is confirmed from the highest strain recorded from strain gage 2 that a crack has initiated at tip B and succeeded by edge C.

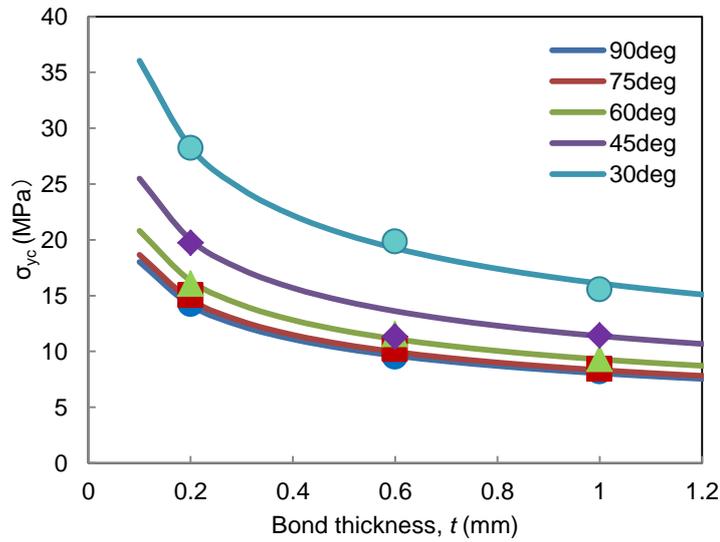


Figure 7. Joint strength prediction for various scarf angles.

Table 5. Failure type and morphology.

Failure type	I. IF	II. IF Transition	III. CF-IF Transition	IV. Rough CF	V. CF
Failure path					
Side view					
Top view					

Table 6. Scarf angle and failure morphology.

Scarf angle	30°	45°	60°	75°	90°
Top view					

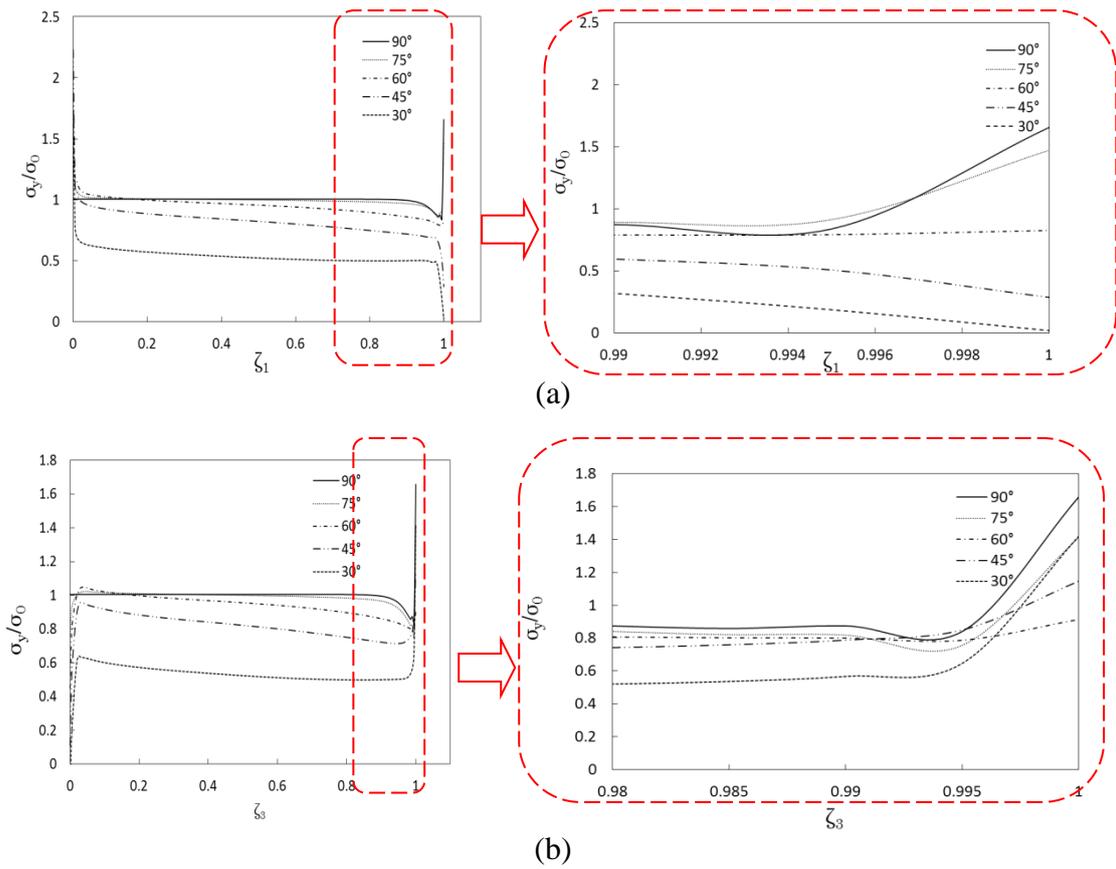


Figure 8. Stress distribution at (a) upper; (b) lower bonding interfaces.

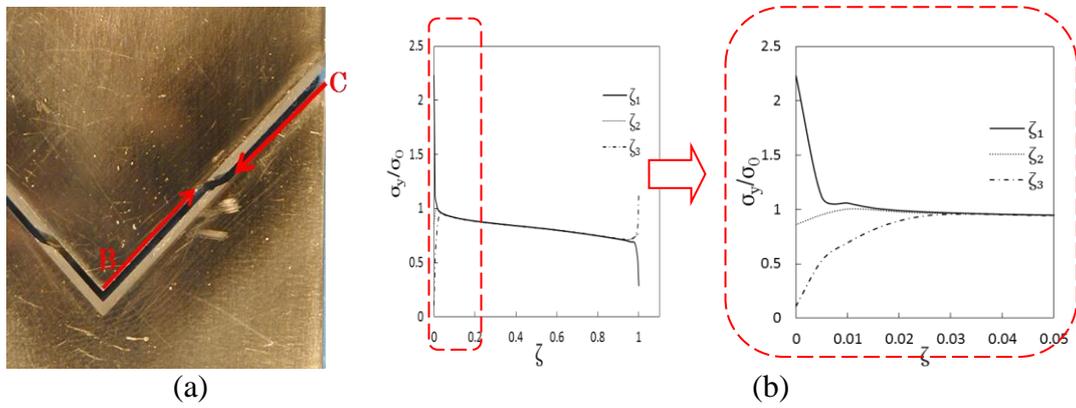


Figure 9. Crack initiation and direction of propagation in 45° specimen.
(a) crack path; (b) stress distribution.

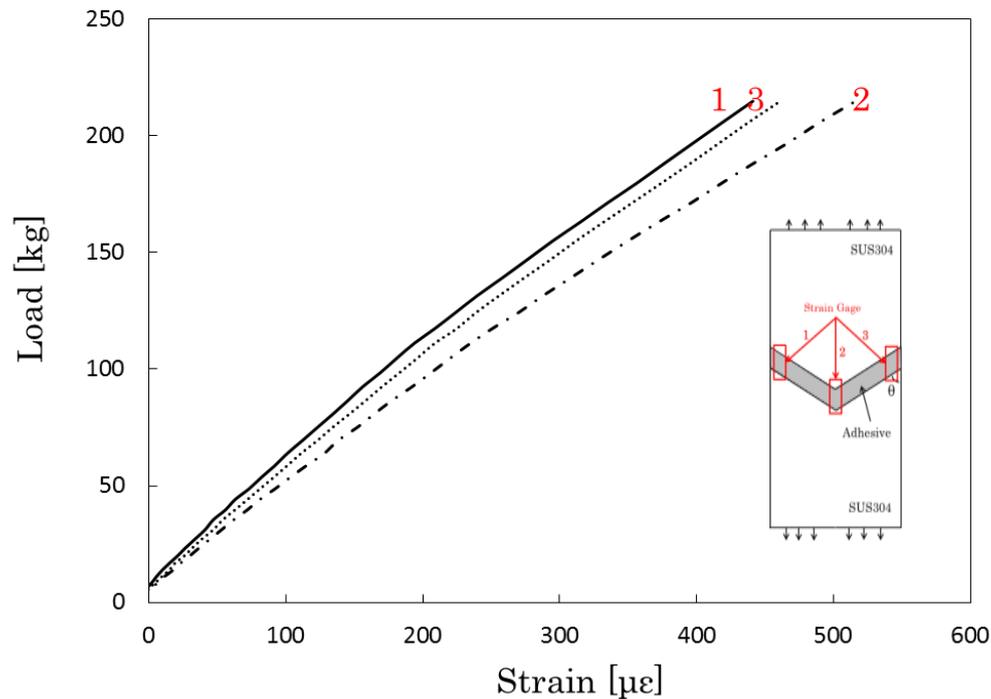


Figure 10. Applied load versus strain for 45° specimen.

CONCLUSIONS

In this study, tensile tests were conducted on V-shaped epoxy adhesive joints having various scarf angles and bond thicknesses. Stress analysis was conducted on V-shaped epoxy adhesive joints of 1.0mm bond thickness with various scarf angles. According to experimental findings, failure stress is greater when the bond thickness is reduced. The direction of the normal stress showed the same tendency as the interface strength properties. Failure morphology can be divided into 5 types, consisting of IF and/or CF. When scarf angle becomes slant, failure morphology changes from CF into IF transition. Failure is governed by the shear stress and strength of specimens which failed, as cohesive failure is greater than those with interfacial failure. Moreover, failure is more dependent on the bond thickness than the scarf angle of V-shaped adhesive joint. For joint strength prediction, a simple failure criterion for V-shaped adhesive joint is proposed and it has considerable potential. The FEA results confirm that cracks will originate at the tip or edge with higher stress singularity. Crack propagation paths depend on stress distribution at interfaces and inside the adhesive layer. It can also be concluded that stress distribution at interfaces and inside the adhesive layer determines the observed failure morphology.

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